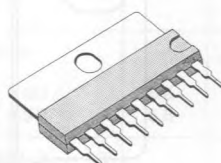


6+6W STEREO AMPLIFIER

The TDA 2007 is a class AB dual Audio power amplifier assembled in single in line 9 pins package, specially designed for stereo application in music centers TV receivers and portable radios. Its main features are:

- High output power
- High current capability
- Thermal overload protection
- Space and cost saving: very low number of external components and simple mounting thanks to the SIP. 9 package.



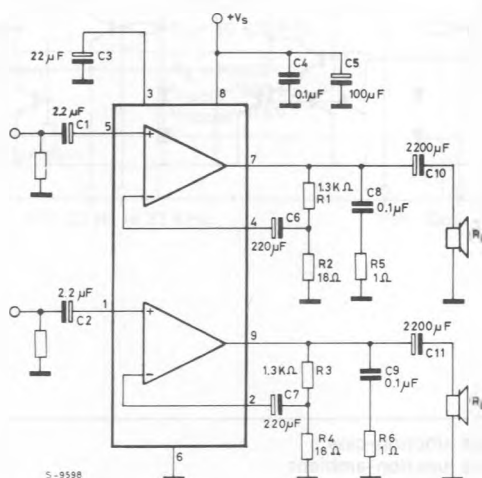
SIP. 9

ORDERING NUMBER: TDA 2007

ABSOLUTE MAXIMUM RATINGS

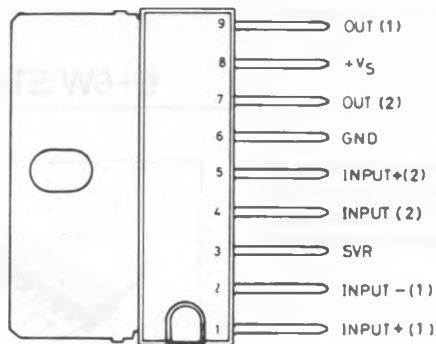
V_s	Supply voltage	28	V
I_o	Output peak current (repetitive $f \geq 20$ Hz)	3	A
I_o	Output peak current (non repetitive, $t = 100 \mu s$)	3.5	A
P_{tot}	Power dissipation at $T_{case} = 70^\circ C$	10	W
T_{stg}, T_j	Storage and junction temperature	-40 to 150	$^\circ C$

STEREO TEST CIRCUIT



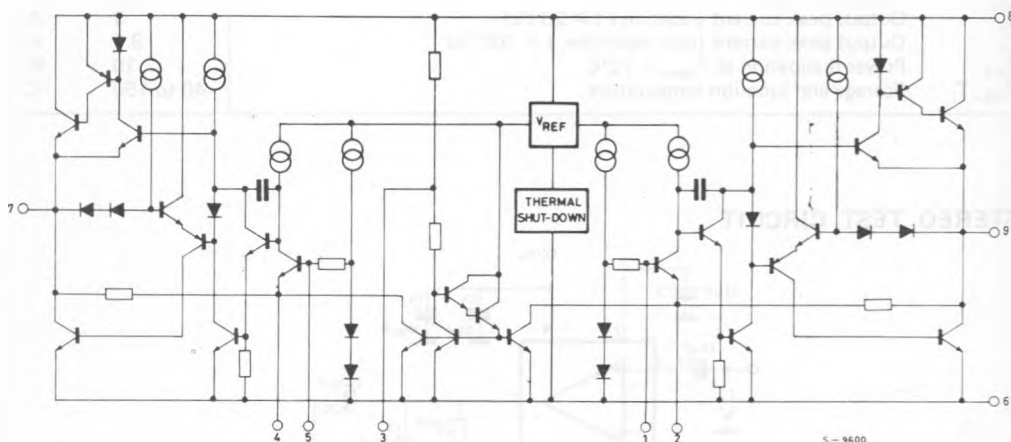
CONNECTION DIAGRAM

(Top view)



5-9599

SCHEMATIC DIAGRAM



5-9600

THERMAL DATA

$R_{th\ j-case}$	Thermal resistance junction-case	max	8	°C/W
$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	70	°C/W

ELECTRICAL CHARACTERISTICS (Refer to the stereo application circuit, $T_{amb} = 25^{\circ}\text{C}$, $V_s = 18\text{V}$, $G_v = 36\text{ dB}$, unless otherwise specified)

Parameters	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage		8		26	V
V_o Quiescent output voltage			8.5		V
I_d Total quiescent drain current			48		mA
P_o Output power (each channel)	$f = 100\text{ Hz to }16\text{ KHz}$ $d = 0.5\%$ $V_s = 18\text{V}$ $R_L = 4\Omega$ $V_s = 22\text{V}$ $R_L = 8\Omega$	5.5 5.5	6 6		W W
d Distortion (each channel)	$f = 1\text{ KHz}$, $V_s = 18\text{V}$, $R_L = 4\Omega$ $P_o = 100\text{ mW to }3\text{W}$		0.1		%
	$f = 1\text{ KHz}$, $V_s = 22\text{V}$, $R_L = 8\Omega$ $P_o = 100\text{ mW to }3\text{W}$		0.05		%
CT Cross talk (°°°)	$R_L = \infty$ $f = 1\text{ KHz}$	50	60		dB
	$R_g = 10\text{ K}\Omega$ $f = 10\text{ KHz}$	40	50		dB
V_i Input saturation voltage (rms)		300			mV
R_i Input resistance	$f = 1\text{ KHz}$	70	200		$\text{K}\Omega$
f_L Low frequency roll off (-3 dB)	$R_L = 4\Omega$, $C_{10} = C_{11} = 2200\text{ }\mu\text{F}$		40		Hz
f_H High frequency roll off (-3 dB)			80		KHz
G_v Voltage gain (closed loop)	$f = 1\text{ KHz}$	35.5	36	36.5	dB
ΔG_v Closed loop gain matching			0.5		dB
e_N Total input noise voltage	$R_g = 10\text{ K}\Omega$ (°)		1.5		μV
	$R_g = 10\text{ K}\Omega$ (°°)		2.5	8	μV
SVR Supply voltage rejection (each channel)	$R_g = 10\text{ K}\Omega$ $f_{\text{ripple}} = 100\text{ Hz}$ $V_{\text{ripple}} = 0.5\text{V}$		55		dB
T_J Thermal shut-down junction temperature			145		$^{\circ}\text{C}$

(°) Curve A.

(°°) 22 Hz to 22 KHz.

(°°°) Optimized test box.

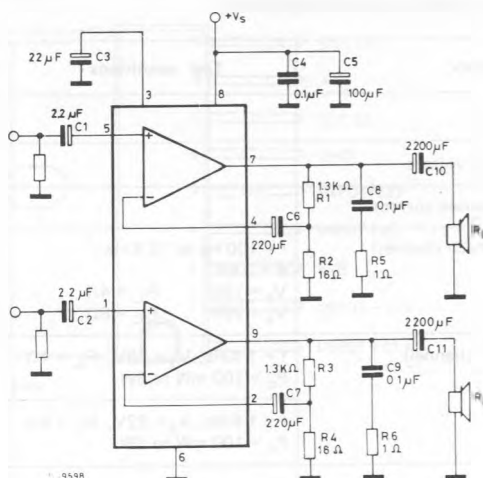
Fig. 1 - Stereo test circuit ($G_v = 36 \text{ dB}$)

Fig. 2 - P.C. board and components layout of the circuit of fig. 1 (1 : 1 scale)

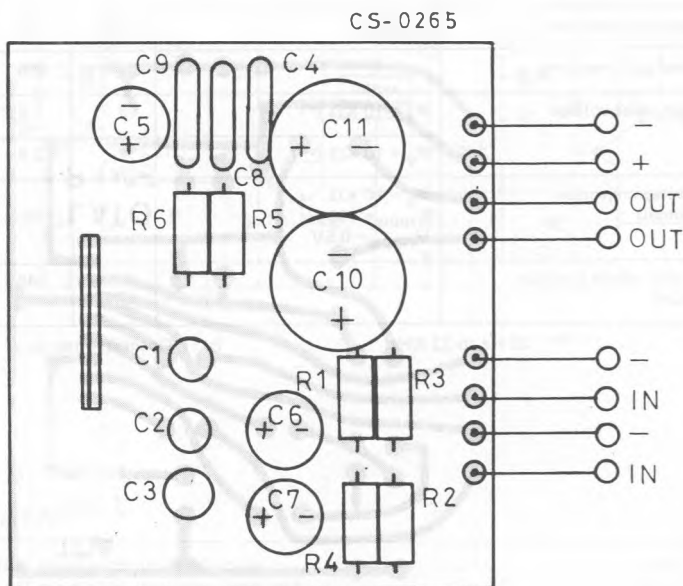


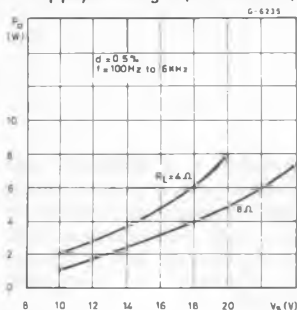
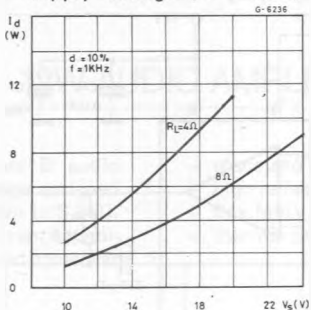
Fig. 3 - Output power vs. supply voltage ($d = 0.5\%$)Fig. 4 - Output power vs. supply voltage ($d = 10\%$)

Fig. 5 - Quiescent current vs. supply voltage

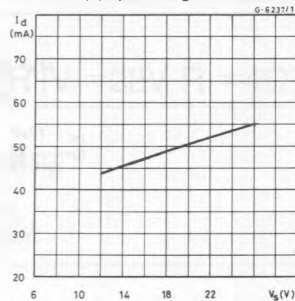


Fig. 6 - Supply voltage rejection vs. value of capacitor C3

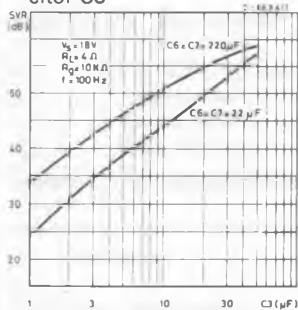


Fig. 7 - Supply voltage rejection vs. frequency

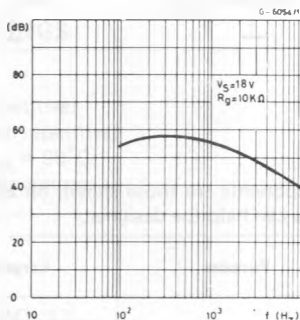


Fig. 8 - Total power dissipation vs. output power

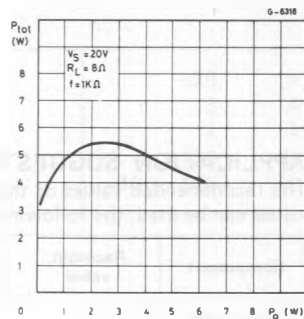


Fig. 9 - Cross-talk vs. frequency

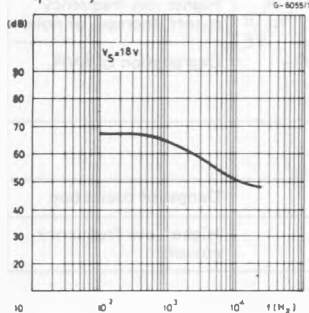


Fig. 10 - Simple short-circuit protection

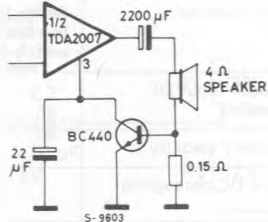
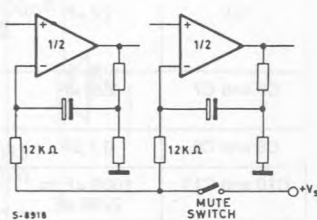
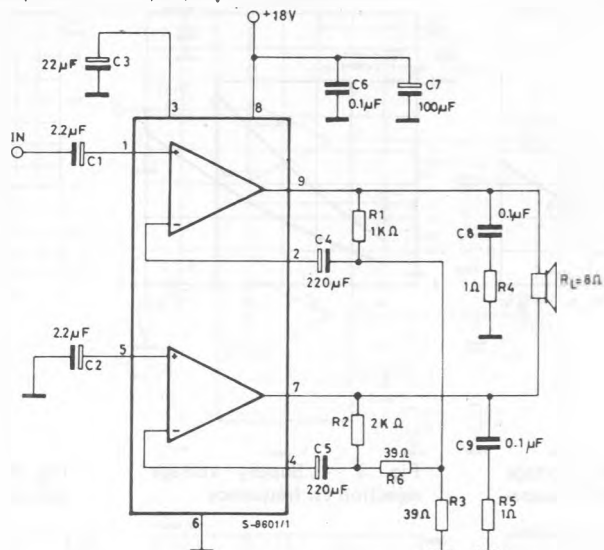


Fig. 11 - Example of muting circuit



APPLICATION INFORMATION

Fig. 12 - 12W bridge amplifier ($d = 0,5\%$, $G_v = 40\text{dB}$)

APPLICATION SUGGESTION

The recommended values of the components are those shown on application circuit of fig. 1. Different values can be used; the following table can help the designer.

Component	Recomm. value	Purpose	Larger than	Smaller than
R1 and R3	1.3 K Ω	Close loop gain setting (*)	Increase of gain	Decrease of gain
R2 and R4	18 Ω		Decrease of gain	Increase of gain
R5 and R6	1 Ω	Frequency stability	Danger of oscillation at high frequency with inductive load	
C1 and C2	2.2 μF	Input DC decoupling	High turn-on delay	High turn-on pop Higher low frequency cutoff. Increase of noise
C3	22 μF	Ripple rejection	Better SVR. Increase of the switch-on time	Degradation of SVR.
C6 and C7	220 μF	Feedback Input DC decoupling		
C8 and C9	0.1 μF	Frequency stability		Danger of oscillation
C10 and C11	1000 μF to 2200 μF	Output DC decoupling		Higher low-frequency cut-off

(*) The closed loop gain must be higher than 26 dB.