

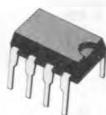
MINIDIP STEREO PREAMPLIFIER

- WIDE SUPPLY VOLTAGE RANGE (3 TO 36V)
- SINGLE OR SPLIT SUPPLY OPERATION
- VERY LOW CURRENT CONSUMPTION (0.8mA)
- VERY LOW DISTORTION
- NO POP-NOISE
- SHORT CIRCUIT PROTECTION

The TDA2320A is a stereo class A preamplifier intended for application in portable cassette

players and high quality audio systems.

The TDA2320A is a monolithic integrated circuit a 8 lead minidip.



Minidip Plastic

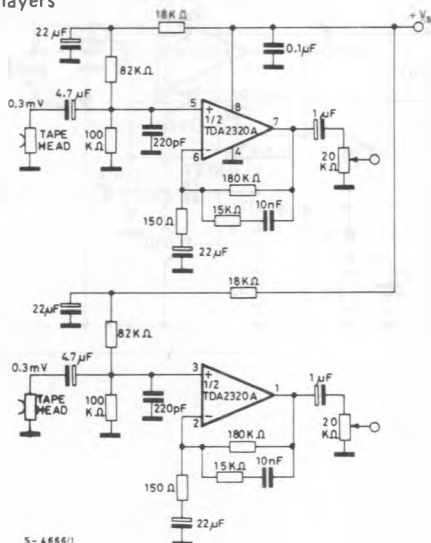
ORDERING NUMBER: TDA 2320A

ABSOLUTE MAXIMUM RATINGS

V_s	Supply voltage	36	V
P_{tot}	Total power dissipation at $T_{amb} = 70^\circ\text{C}$	400	mW
$T_{stg, j}$	Storage and junction temperature	-40 to 150	$^\circ\text{C}$

TYPICAL APPLICATION:

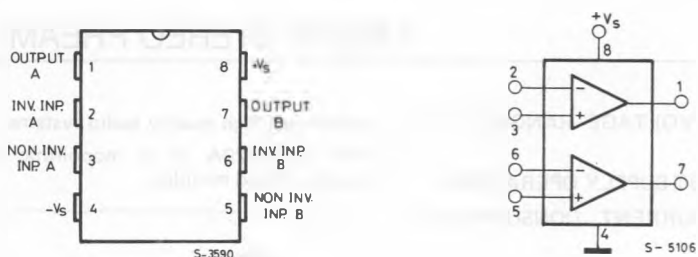
Stereo preamplifier for cassette players



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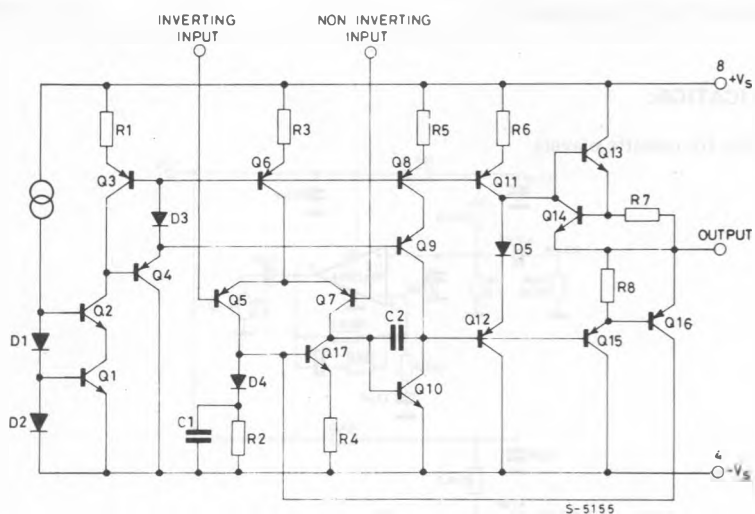
CONNECTION AND BLOCK DIAGRAM

(top view)



SCHEMATIC DIAGRAM

(one section)



TEST CIRCUITS

Fig. 1

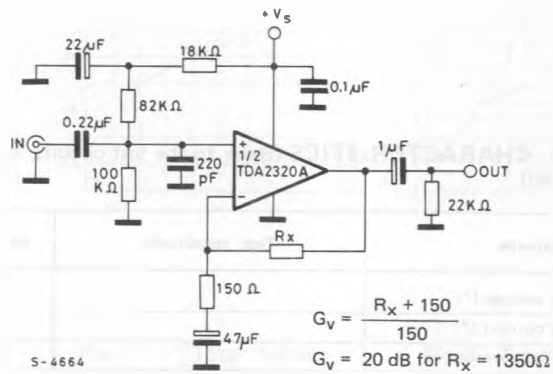
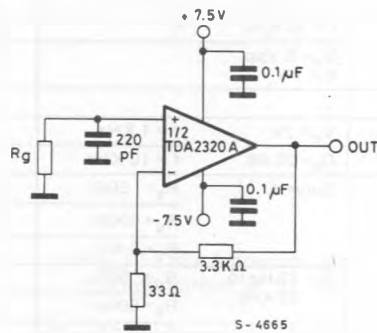


Fig. 2



THERMAL DATA

$R_{th\ j-amb}$	Thermal resistance junction-ambient	max	200	°C/W
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ELECTRICAL CHARACTERISTICS (Refer to the test circuits, $V_s = 15V$, $T_{amb} = 25^\circ C$, unless otherwise specified)

Parameter	Test conditions	Min.	Typ.	Max.	Unit
V_s Supply voltage (*)		3		36	V
I_s Supply current (*)			0.8	2	mA
I_b Input bias current			150	500	nA
V_{os} Input offset voltage	$R_g < 10\ K\Omega$		1	5	mV
I_{os} Input offset current			10	50	nA
G_v Open loop voltage gain	$V_s = 15V$	$f = 333\ Hz$	80		dB
		$f = 1\ KHz$	70		
		$f = 10\ KHz$	50		
	$V_s = 4.5V$	$f = 1\ KHz$	70		
V_o Output voltage swing (*)	$f = 1\ KHz$	$V_s = 15V$	13		Vpp
	$R_L = 600\Omega$	$V_s = 4.5V$	2.5		
B Gain-bandwidth product	$f = 20\ KHz$	1.5	2.5		MHz
BW Power bandwidth (*)	$V_o = 5\ Vpp$ $d = 1\%$	40	70		KHz
SR Slew rate (*)		1	1.6		V/ μS
d Distortion (*)	$V_o = 2V$	$f = 1\ KHz$	0.03		%
	$G_v = 20\ dB$	$f = 10\ KHz$	0.08		
e_N Total input noise voltage (**)	Curve A	$R_g = 50\Omega$	1		μV
		$R_g = 600\Omega$	1.1	1.4	
		$R_g = 5\ K\Omega$	1.5		
	B = 22 Hz to 22 KHz	$R_g = 50\Omega$	1.3		μV
		$R_g = 600\Omega$	1.5		
		$R_g = 5\ K\Omega$	2		
	$f = 1\ KHz$	$R_o = 600\Omega$	9		nV/ $\sqrt{Hz}$
Cs Channel separation (**)	$f = 1\ KHz$		100		dB
SVR Supply voltage (**) rejection	$f = 100\ Hz$		80		dB

(*) Test circuit of fig. 1.

(**) Test circuit of fig. 2.

Fig. 3 - Supply current vs. supply voltage

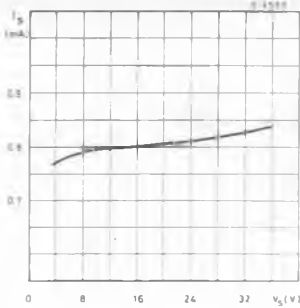


Fig. 4 - Supply current vs. ambient temperature

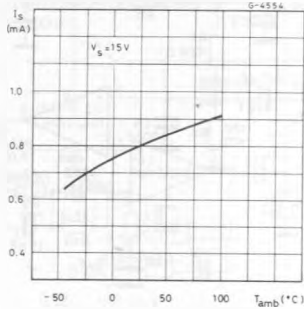


Fig. 5 - Output voltage swing vs. load resistance

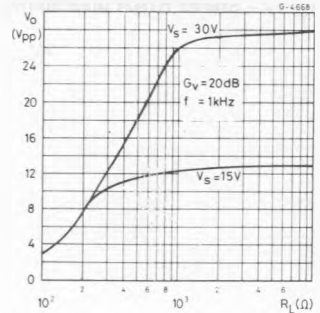


Fig. 6 - Power bandwidth

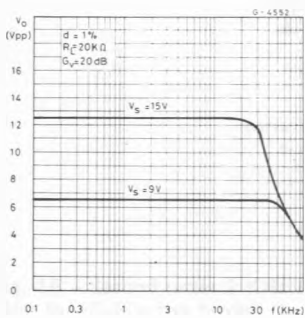


Fig. 7 - Total harmonic distortion vs. output voltage

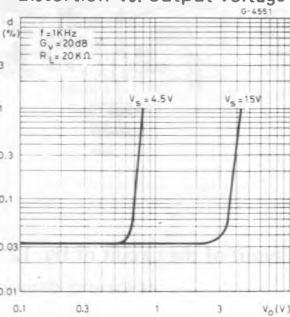


Fig. 8 - Total input noise vs. source resistance

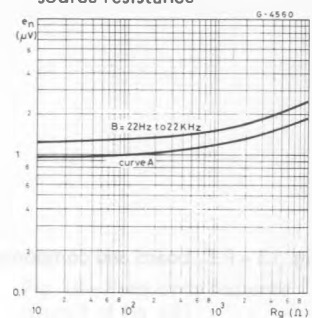


Fig. 9 - Noise density vs. frequency

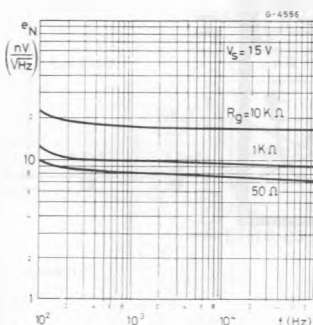


Fig. 10 - RIAA preamplifier response (circuit of fig. 12)

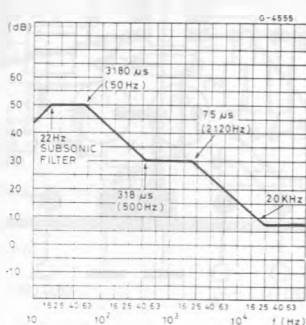
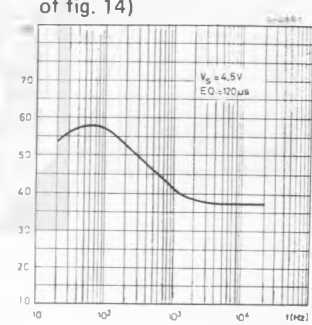
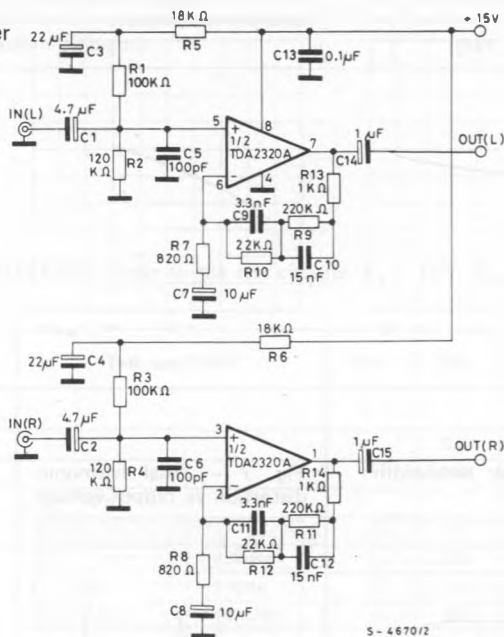


Fig. 11 - Tape preamplifier frequency response (circuit of fig. 14)



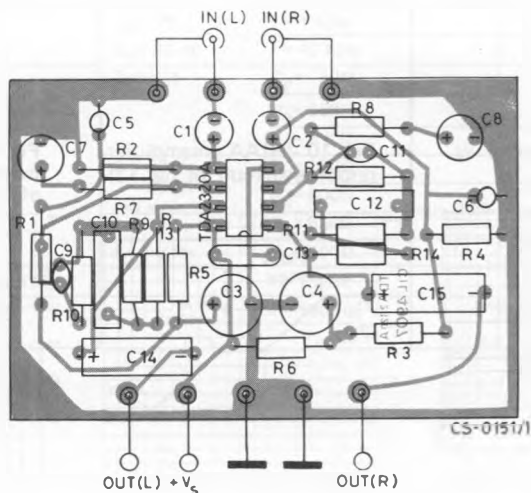
APPLICATION INFORMATION

Fig. 12 - Stereo RIAA preamplifier



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Fig. 13 - P.C. board and components layout of the circuit of fig. 12



APPLICATION INFORMATION (continued)

Fig. 14 – Stereo preamplifier for Walkman cassette players

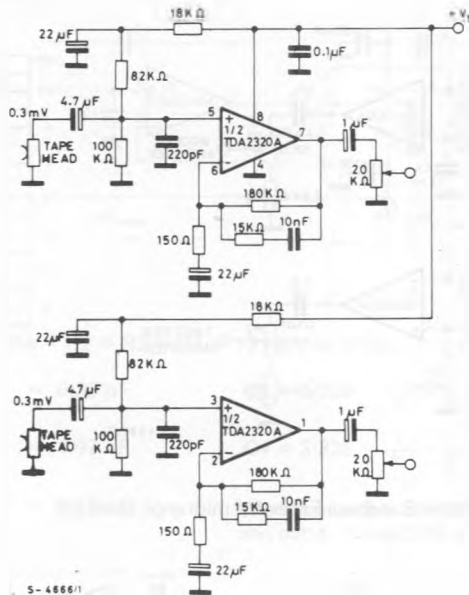


Fig. 15 – Second order 2 KHz Butterworth crossover filter for Hi-Fi active boxes

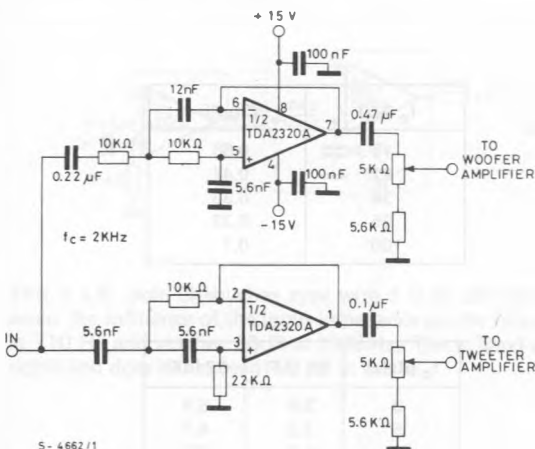
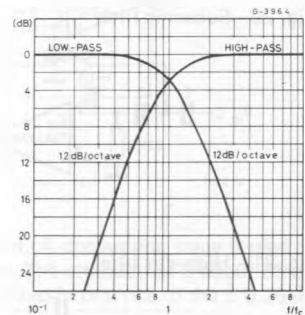
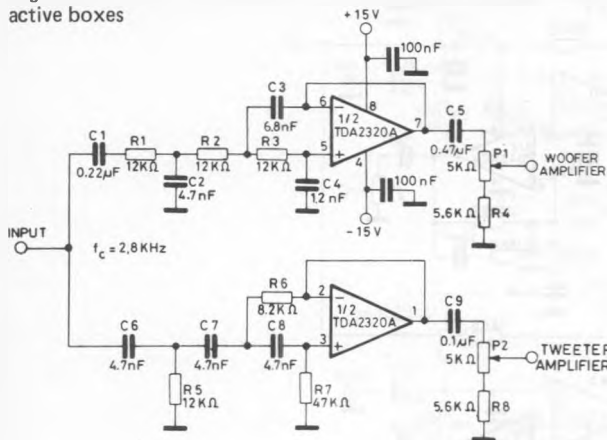


Fig. 16 – Frequency response (circuit of fig. 15)



APPLICATION INFORMATION (continued)

Fig. 17 - Third order 2.8 KHz Bessel crossover filter for Hi-Fi active boxes



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Fig. 18 - Frequency response (circuit of fig. 17)

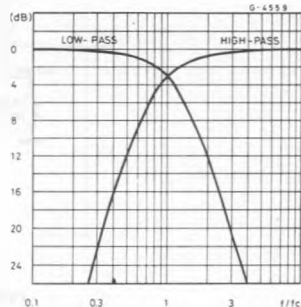
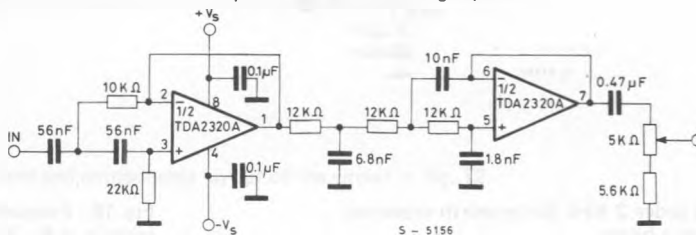
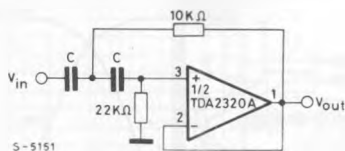


Fig. 19 - 200 Hz to 2 KHz Active Bandpass Filter for midrange speakers



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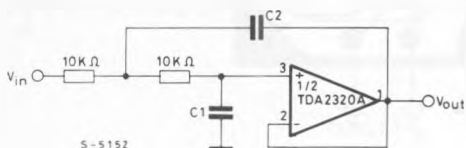
Fig. 20 - Subsonic filter



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f_c (Hz)	C (μ F)
15	0.68
22	0.47
30	0.33
55	0.22
100	0.1

Fig. 21 - High-cut filter

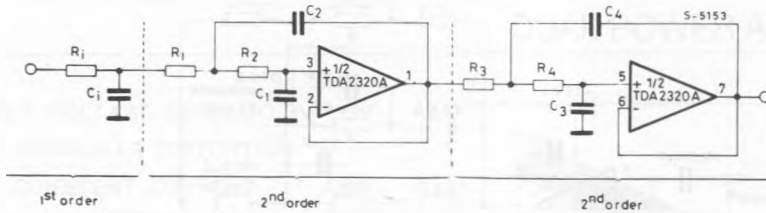


S - 5152

f_c (KHz)	C1 (nF)	C2 (nF)
3	3.9	6.8
5	2.2	4.7
10	1.2	2.2
15	0.68	1.5

APPLICATION INFORMATION (continued)

Fig. 22 - Fifth order 3.4 KHz low-pass Butterworth filter



For $f_c = 3.4 \text{ KHz}$ and $R_1 = R_1 = R_2 = R_3 = R_4 = 10 \text{ K}\Omega$, we obtain:

$$C1 = 1.354 \cdot \frac{1}{R} \cdot \frac{1}{2 \pi f_c} = 6.33 \text{ nF}$$

$$C3 = 0.309 \cdot \frac{1}{R} \cdot \frac{1}{2 \pi f_c} = 1.45 \text{ nF}$$

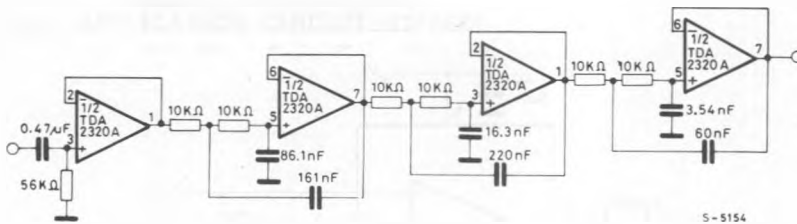
$$C1 = 0.421 \cdot \frac{1}{R} \cdot \frac{1}{2 \pi f_c} = 1.97 \text{ nF}$$

$$C4 = 3.325 \cdot \frac{1}{R} \cdot \frac{1}{2 \pi f_c} = 15.14 \text{ nF}$$

$$C2 = 1.753 \cdot \frac{1}{R} \cdot \frac{1}{2 \pi f_c} = 8.20 \text{ nF}$$

The attenuation of the filter is 30 dB at 6.8 KHz and better than 60 dB at 15 KHz.

Fig. 23 - Sixth-pole 355 Hz low-pass filter (Chebychev type)



This is a 6-pole Chebychev type with $\pm 0.25 \text{ dB}$ ripple in the passband. A decoupling stage is used to avoid the influence of the input impedance on the filter's characteristics. The attenuation is about 55 dB at 710 Hz and reaches 80dB at 1065 Hz. The in band attenuation is limited in practice to the $\pm 0.25 \text{ dB}$ ripple and does not exceed $1/2 \text{ dB}$ at $0.9 f_c$.

APPLICATION INFORMATION (continued)

Fig. 24 – Three band tone control

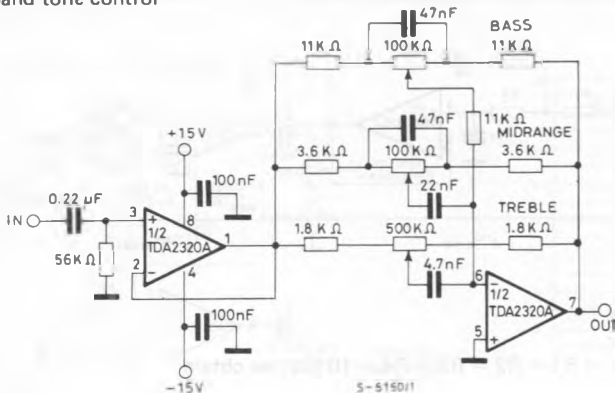


Fig. 25 – Frequency response of the circuit of fig. 24.

- A : all controls flat
- B : bass & treble boost, mid flat
- C : bass & treble cut, mid flat
- D : mid boost, bass & treble flat
- E : mid cut, bass & treble flat

